

Effect of surface hardness and roughness produced by turning on the torsion mechanical properties of annealed AISI 1020 steel

Efecto de la dureza y rugosidad superficial producidos por torneado en las propiedades mecánicas a torsión del acero AISI 1020 recocido

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ARTICLE INFO

Received May 23, 2017 Accepted August 20, 2017 **ABSTRACT:** This paper presents the results of experimental work carried out to study the influence of surface integrity, measured as hardness (HV) and roughness (Ra) on torsional properties of annealed AISI 1020 steel machined by turning using carbide insert tools. The results showed a reduction in ductility when hardness and roughness increase, caused by the plastic deformation induced after machining. It was shown that the shear yield strength increases, as a consequence of the material strengthening by work-hardening and the rise of stress concentrators. Further, the ultimate shear strength increases with surface hardness, having the opposite effect when the surface roughness caused greater stress concentration.

KEYWORDS

AISI 1020, ductility, strength, hardness, roughness, torsion

AISI 1020, ductilidad, esfuerzo, dureza, rugosidad, torsión

RESUMEN: Este artículo presenta los resultados del trabajo experimental llevado a cabo para estudiar la influencia de la integridad superficial, medida como dureza (HV) y la rugosidad (Ra) en las propiedades a torsión del acero AISI 1020 recocido torneado con herramientas de corte con inserto de carburo. Los resultados mostraron una reducción de la ductilidad con el aumento de la dureza y rugosidad, causado por la deformación plástica inducida después del mecanizado. Se demostró que el límite elástico de cizalladura aumenta como consecuencia del endurecimiento del material y el incremento de concentradores de esfuerzos. Además, la resistencia máxima a la cizalladura aumenta con la dureza de la superficie, pero tiene el efecto contrario cuando la rugosidad de la superficie provoca una mayor concentración de esfuerzos.

1. Introduction

In machinery, parts such as shafts, axles, and twist drills are subjected to torsional loading in service, resulting in possible deformation or fracture that may affect their proper operation. Hence, to improve certain properties, such as increasing the fatigue strength, stresses are intentionally introduced in the material.

Among all conventional methods available in the manufacturing industry, machining continues to dominate in the production of these components. Particularly, turning is a machining process that produces cylindrical parts using a single-point cutting tool to remove material on an external surface of a workpiece.

A surface is described in simple terms as the outermost layer of an entity [1]. Surface integrity has a direct effect on the quality and functionality of produced parts and is a

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relevant parameter used for evaluating a machined surface. Many mechanical components require special attention on the surface roughness because it affects the appearance, reliability, and function of the product. Meanwhile, these components also need to have a high surface hardness to resist wear and plastic deformation during services. Therefore, an improved control of surface integrity is considered to be of importance.

Several factors affect machined surface roughness, such as tool geometry, tool wear, coolant and cutting parameters. The influence of tool geometry by means of the nose radius has been previously investigated, proving that high radius values cause rough surfaces [2, 3]. According to a previous experimental research cutting with a worn tool also resulted in worse roughness [4]. Works conducted to analyze the effect of coolant showed that higher surface roughness was achieved on components machined without coolant, as compared to those with a supply of coolant [5, 6]. Finally, there is an abundance of literature describing the relation of cutting parameters on surface roughness. Results from these studies indicated that a higher feed rate and depth of cut increase the surface finish values while cutting speed had the opposite effect on aluminum [6, 7], brass alloys [8], carbon alloy steels [9-12], EN-31 steel [13] and stainless steels [14].

DOI: 10.17533/udea.redin.n84a07

Prior research also provides experimental results on the influence of the turning process on the surface hardness of machined parts. For example, cutting edge wear affects the hardness as greater values were found when machining with worn tools [15]. Meanwhile, most efforts have been made to analyze how cutting parameters affect the surface hardness. In the majority of them, it was found that higher values of hardness are obtained when increasing the depth of cut and feed rate, while on the other hand, cutting speed had the opposite effect on turning of stainless steels [16- 18] and nickel alloys [19]. However, deviations from these results were reported for carbon alloy steels [9], alloyed steels [20], stainless steels [21] and titanium alloys [15].

From the background literature, it is observed that extensive research has been made covering the relation of the turning process on surface hardness and roughness. Nevertheless, there are no attempts to describe or analyze the influence of surface integrity on mechanical properties of machined components. Taking into consideration the importance of quality and functionality of produced parts, this research area is well worth developing. Therefore, the aim of the present investigation is to study the effects of surface hardness (HV) and surface roughness (Ra) induced after turning on the torsion properties of annealed AISI 1020 steel.

2. Experimental procedure

The material used in this work was a round bar of commercial AISI 1020 steel (0.18 ± 0.01% C, 0.035 ± 0.001% S, and 0.40 ± 0.01% Mn) with a diameter of 31.75 mm, cut in cylinders of 170 mm in length. These were later annealed for 1 h at 910 °C and cooled slowly inside the furnace.

The work samples were machined in a numerically controlled lathe; using ISO code - DCMT11T308MU carbide inserts and with an abundant quantity of water-soluble oil as coolant. To ensure same cutting conditions and guarantee the absence of changes in the surface properties of the material due to the tool wear [15, 22], a new insert's edge was used for each test.

The tests were designed in a factorial arrangement technique of variables [23], with three levels of depth of cut, three levels of feed rate, and two levels for the cutting speed, for 18 random combinations in total. The minimum and maximum limits shown in Table 1 were restricted by the lathe and were selected based on previous experience with AISI 1020 steel [11].

Table 1 **Parameters used in the turning of the samples**

The specimens for roughness and torsion experiments were turned in the geometry and required dimension shown in Figure 1, with a central cylindrical test zone of 10 mm in diameter and 100 mm in length, according to the recommendations given by the ASTM A938 – 07 standard [24]. Meanwhile, the hardness samples were obtained by turning 15 mm in length from the edge of the annealed cylinders and later cut perpendicular to the axis direction, within the machined length. The resulting cross-sectional areas were later prepared according to ASTM E3-11 standard metallographic techniques [25].

Figure 1 **Torsion specimen's geometry and dimensions**

A Vickers microhardness profile was measured for each sample on the cross-section starting from the edge along the radius, with 70 µm spacing. For each distance, three indentations were made, using a Buehler Vickers tester and carried out at a load of 200 gf for 15 s according to ASTM E384-11 standard [26]. The average maximum hardness reached near the surface was studied since it is the value exposed to the higher loads on a component in torsion conditions.

The surface roughness data for each machined test specimen was collected by using a Mitutoyo, Surftest 211 Profilometer, positioning the instrument perpendicular to the feed marks. For every sample, four measurements at randomly chosen locations were made to calculate the average value of Ra.

Finally, these specimens were subject to torsion test performed on a free-end torsion machine, by deforming until fracture at a constant strain rate of 2.3×10^{-2} s⁻¹ and a rotational speed of 8.6 rpm, according to the ASTM A938 - 07 standard [24]. During the entire test the actual torque and the torsion angle of the specimens were measured.

3. Results and discussion

After the turning process, changes in the measured values of surface hardness and roughness of the specimens were expected [9, 10]. It was found that the surface hardness increases with the increase of all the studied parameters, while the surface roughness increased for higher feed rates and lower cutting speeds.

It is very important to note in Figure 2 how cutting speed remarkably affects the responses, as the slope with a cutting speed of 70 m/min is larger than with 20 m/min. Therefore, surface roughness grows quite faster under the

lower cutting speed, while hardness increases faster under the higher speed. Statistical Pareto-ANOVA analysis of the individual influence of the control factors using Minitab, demonstrated that cutting speed was the independent parameter that had the most effect on the responses with a contribution near 70% to the overall turning parameters, followed by the feed rate; the depth of cut had a little substantial effect. This is in agreement with the findings of previous researchers [11].

Figure 2 **Surface microhardness versus roughness for turned annealed AISI 1020 steel**

It is clear that machining has an impact on the hardness and roughness of the workpiece surface layer, and both are a function of the cutting parameters. During turning, the cutting force required to cause the tearing of the chips as the tool advances induces a severe plastic deformation at surface and subsurface layers. This deformation results in cold working that affects the metal ductility, hardness, and strength [1]. Meanwhile, a subsurface material fracture occurs due to the violent deformation of the chip, which generates worse surface roughness [5]. The shape, size, and depth of the surface grooves also alter the metal properties.

In materials science, ductility is known as the ability of a solid material to undergo permanent deformation without fracturing; it may be expressed as fracture strain ($\varepsilon_{_{\rm f}}$) or percent reduction in area. In Figure 3, it is shown that a reduction in fracture strain occurred with increasing the surface hardness of the specimens, for fixed cutting speeds. Due to the plastic deformation induced after machining [9], it was expected that the material had been extended through part of its allowed plastic deformation, thus the ductility of the hardened workpieces should decrease.

For comparison purposes, Figure 3 also shows the significant influence of cutting speed on ductility, where greater values of fracture strain were achieved with the higher speed. The reason might be that as cutting speed decreases the surface roughness increases, resulting in

localized concentration sites for crack nucleation [11]. Therefore, the reduction in area and propagation of cracks produces the earlier fracture of the workpiece. This tendency was the same for all the measured values of roughness, as shown in Figure 4.

Figure 4 **Fracture strain plotted against surface roughness**

The effect of surface hardness on the shear yield strength is shown in Figure 5(a), where higher values of shear yield strength were obtained with increasing the hardness, for fixed cutting speeds. This is related to the fact that an augmentation of the work-hardened surface, caused by the forces acting between the surface layer and the tool, results in the strengthening of the material by plastic deformation [1]. The combined effect of surface roughness produced by the different cutting speeds is shown in Figure 5(b). It can be observed that the slope with a cutting speed of 20 m/min is lower than for 70 m/min. Thus, a smaller increase in surface roughness will lead to a higher increase in strength, which is caused by the rise of stress concentrators [11].

surface, (a) hardness; and (b) roughness

From Figure 6(a), it can be seen that as surface hardness increased, the values of ultimate shear stress also increase for a cutting speed of 70 m/min. This is in agreement with the previous results for shear yield strength, as a consequence of the strengthening of the material by workhardening. However, a deviation from this trend is shown for the cutting speed of 20 m/min, where lower values of maximum shear stress resulted when the roughness increased. This behavior is in alignment with the significant influence of cutting speed on surface roughness (Figure 6(b)). In all torsion tests, maximum values of shear stress were achieved at reaching fracture of the samples. Therefore, stress concentrators originated from higher values of surface roughness might speed up the fracture mechanisms, lowering the ultimate shear stress [11].

Figure 6 **Ultimate shear strength plotted against surface, (a) hardness; and (b) roughness**

4. Conclusions

Within the limitations of this experimental study on the relationship between surface hardness and roughness, and torsion mechanical properties of annealed AISI 1020 steel, the following conclusions can be drawn:

- Reduction in ductility was observed when surface hardness and roughness increased, as a consequence of the changes induced after machining.
- The shear yield strength is surface texture dependent; as increasing the surface hardness and roughness have the effect of increasing the strength, which can be attributed to the strengthening of the material and the rise of stress concentrators.
- The surface hardness determines the ultimate shear strength, increasing its values, except where the surface roughness causes greater stress concentration having the opposite effect.

5. References

- 1. J. P. Davim, *Surface Integrity in Machining*, 1*st* ed. London, England: Springer-Verlag, 2010.
- 2. M.Y. Wang and T.S. Lan, "Parametric Optimization on Multi Objective Precision Turning using Grey Relational Analysis," *Inform. Technol. J.*, vol. 7, no. 7, pp. 1072- 1076, 2008.
- 3. K. S. Saad, "Studying the Effect of Tool Nose Radius on Work Piece Run Out and Surface Finish," *Eng. Technol. J.*, vol. 27, no. 2, pp. 256-261, 2009.
- 4. H. J. Amorim and A. O. Kunrath, "Study of the Relationship Between Tool Wear and Surface Finish in Turning with Carbide Tool," *Adv. Mater. Res.*, vol. 902, pp. 95-100, 2014.
- 5. P. Deepakkumar and M. Sadaiah, "Investigations on Finish Turning of AISI 4340 Steel in Different Cutting Environments by CBN Insert," *Int. J. Eng. Sci. Technol.*, vol. 3, no. 10, pp. 7690-7706, 2011.
- 6. D. Deepak and B. Rajendra, "Investigations on the Surface Roughness Produced in Turning of AL6061 (ascast) by Taguchi Method," *Int. J. Res. Eng. Technol.*, vol. 4, no. 8, pp. 295-298, 2015.
- 7. B. Das, R.N. Rai, and S. C. Saha, "Analysis of Surface Roughness on Machining of AL-5CU Alloy in CNC Lathe Machine," *Int. J. Res. Eng. Technol.*, vol. 2, no. 9, pp. 296- 299, 2013.
- 8. S. G. Hussein, "An Experimental Study of the Effects of Coolant Fluid on Surface Roughness in Turning Operation for Brass Alloy," *J. Eng.*, vol. 20, no. 3, pp. 96- 104, 2014.
- 9. H. Sasahara, "The Effect on Fatigue Life of Residual Stress and Surface Hardness Resulting from Different Cutting Conditions of 0.45%C Steel," *Int. J. Mach. Tools Manuf.*, vol. 45, pp. 131–136, 2005.
- 10. H. Gokkaya and M. Nalbant, "The Effects of Cutting Tool Geometry and Processing Parameters on the Surface Roughness of AISI 1030 steel," *Mater Des.*, vol. 28, pp. 717-721, 2007.
- 11. A. H. Suhail, N. Ismail, S. V. Wong, and N. A. Abdul, "Optimization of Cutting Parameters Based on Surface Roughness and Assistance of Workpiece Surface Temperature in Turning Process," *Am. J. Eng. Appl. Sci.*, vol. 3, no. 1, pp. 102-108, 2010.
- 12. N. Satheesh, A. Shetty, A. Shetty, A. K, and H. Shetty, "Effect of Spindle Speed and Feed Rate on Surface Roughness of Carbon Steels in CNC Turning," *Procedia Eng*, vol. 38, pp. 691 – 697, 2012.
- 13. L. B. Abhang and M. Hameedullah, "Modeling and Analysis for Surface Roughness in Machining EN-31

Steel using Response Surface Methodology," *Int. J. Appl. Res. Mech. Eng.*, vol.1, no. 1, pp. 33-38, 2011.

- 14. K. Kandananond, "The Determination of Empirical Model for Surface Roughness in Turning Process Using Design of Experiment," *Wseas Trans. Sys.*, vol. 8, no. 10, pp. 1135-1144, 2009.
- 15. C. H. Che-Haron and A. Jawaid, "The effect of Machining on Surface Integrity of Titanium Alloy Ti–6% Al–4% V," *J. Mater. Process. Technol.*, vol. 166, pp. 188-192, 2005.
- 16. G. H. Senussi, "Interaction Effect of Feed Rate and Cutting Speed in CNC - Turning on Chip Micro - Hardness of 304 - Austenitic Stainless Steel," *World Acad. Sci. Eng. Techno.* vol. 28, pp. 121-126, 2007.
- 17. G. Krolczyk, P. Nieslony, and S. Legutko, "Microhardness and Surface Integrity in Turning Process of Duplex Stainless Steel (DSS) for Different Cutting Conditions," *J. Mater. Eng. Perform.*, vol. 23, no. 3, pp. 859–866, 2014.
- 18. P. M. Patil, R. V. Kadi, S. T. Dundur, and A. S. Pol, "Effect of Cutting Parameters on Surface Quality of AISI 316 Austenitic Stainless Steel in CNC Turning," *Int. Res. J. Eng. Technol.*, vol. 02, no. 4, pp. 1453-1460, 2015.
- 19. R. S. Pawade, S. S. Joshi, and P. K. Brahmankar, "Effect of Machining Parameters and Cutting Edge Geometry on Surface Integrity of High-speed Turned Inconel 718," *Int. J. Mach. Tools Manuf.*, vol. 48, no. 1, pp. 15–28, 2008.
- 20. A. Javidi, U. Rieger, and W. Eichlseder, "The Effect of Machining on the Surface Integrity and Fatigue Life," *Int. J. Fatigue.*, vol. 30, no. 10, pp. 2050–2055, 2008.
- 21. M. Cebron, F. Kosel, and J. Kopac, "Effect of Cutting on Surface Hardness and Residual Stresses for 12-Mn Austenitic Steel," *J. Achiev. Mat. Manuf. Eng.*, vol. 55, no. 1, pp. 80-89, 2012.
- 22. A. R. C., Sharman, J. I., Hughes, and K. Ridgway, "An Analysis of the Residual Stresses Generated in Inconel 718TM when Turning," *J. Mater. Process. Technol.*, vol. 173, pp. 359-367, 2006.
- 23. D. C. Montgomery, Design and Analysis of Experiments. 8th ed. New York, USA: Wiley, 2012. pp. 65-102.
- 24. ASTM A938-07, Standard Test Method for Torsion Testing of Wire, 2013. [Online]. Available: http://www. astm.org. Accessed on: Apr. 12, 2017.
- 25. ASTM E3-11, Standard Guide for Preparation of Metallographic Specimens, 2011. [Online]. Available: http://www.astm.org. Accessed on: Apr. 12, 2017.
- 26. ASTM E384-11, Standard Test Method for Knoop and Vickers Hardness of Materials, 2011. [Online]. Available: http://www.astm.org. Accessed on: Apr. 12, 2017.